



# Reinforced Concrete Design I

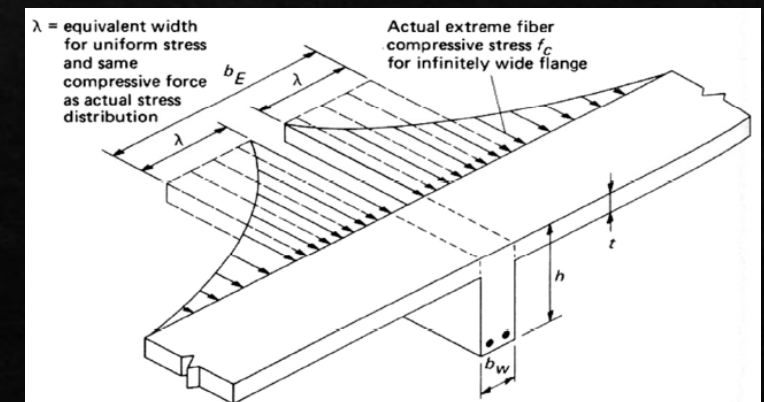
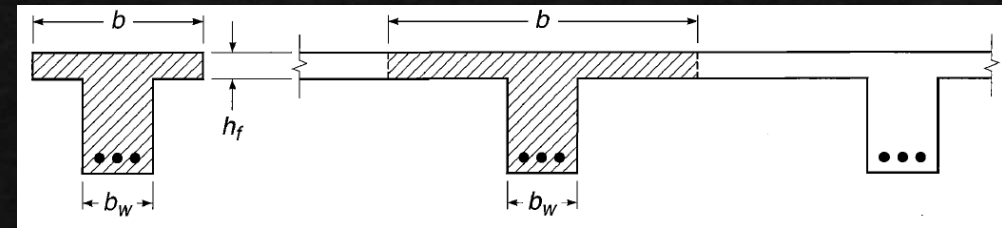
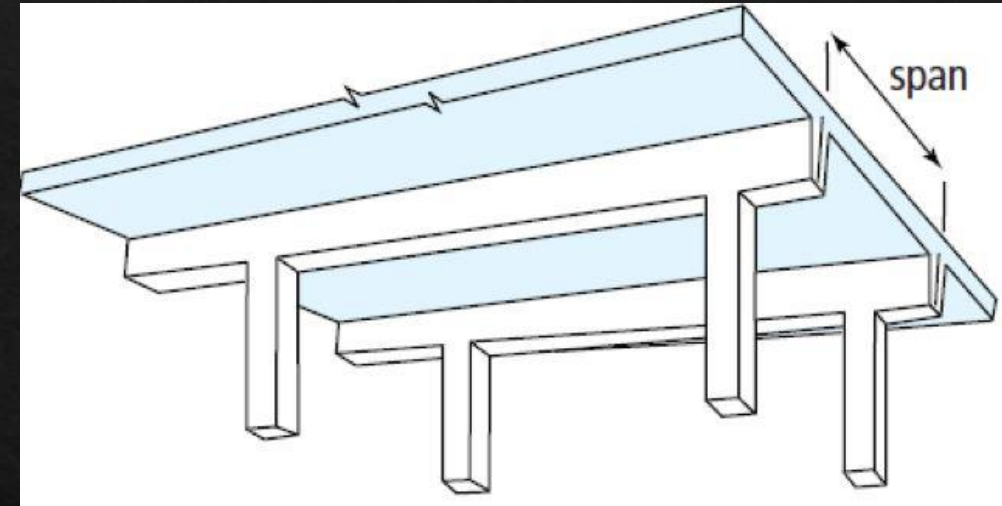
## ENCE 335

Analysis and design of T-beams

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# What are T-section beams

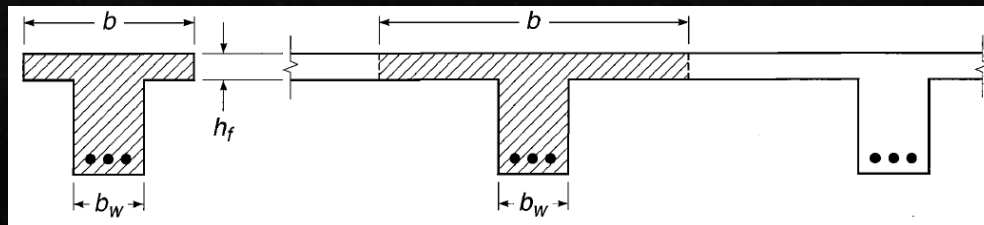
- ◆ In most cases, Slabs and beams are cast at the same time
- ◆ Forms are built for the beams' sides and bottoms as well as the bottom of the slab
- ◆ This is called Monolithic construction
- ◆ In This case, part of the slab (its transverse direction) will resist comp. forces with the upper part of the beam.
- ◆ This part of the slab forms the Flanges of the beam and the drop part of the beam is Stem or Web.
- ◆ The resulting cross-section is T-Shaped



# What are T-section beams

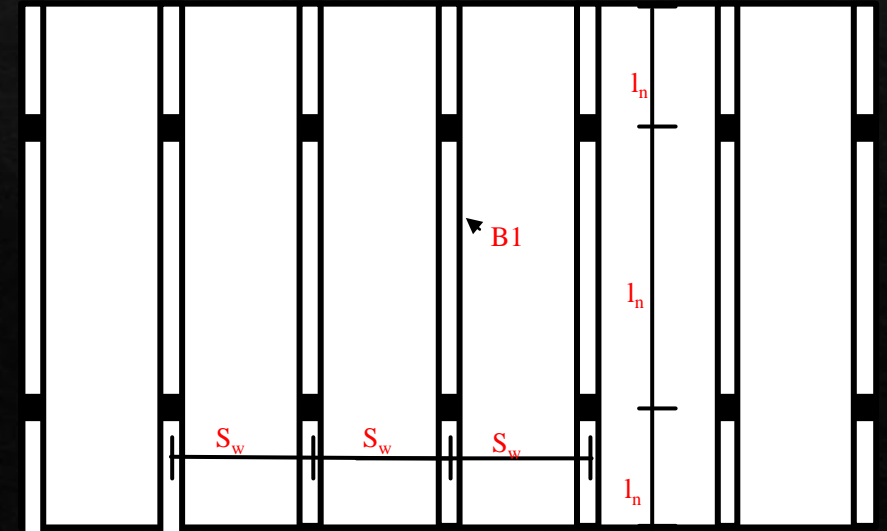
## ◇ Effective width

- ◇ For non-prestressed T-beams supporting monolithic or composite slabs.
- ◇ The effective flange width  $b_f$  shall include the beam web width  $b_w$  plus an effective overhanging flange width in accordance with Table 6.3.2.1
- ◇ Where  $h$  is the slab thickness and  $s_w$  is the clear distance to the adjacent web.



**Table 6.3.2.1—Dimensional limits for effective overhanging flange width for T-beams**

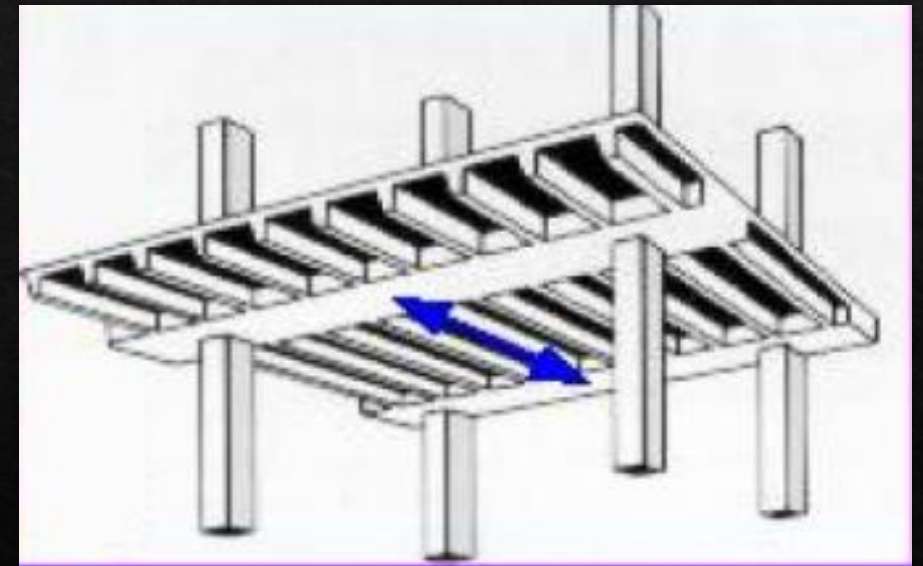
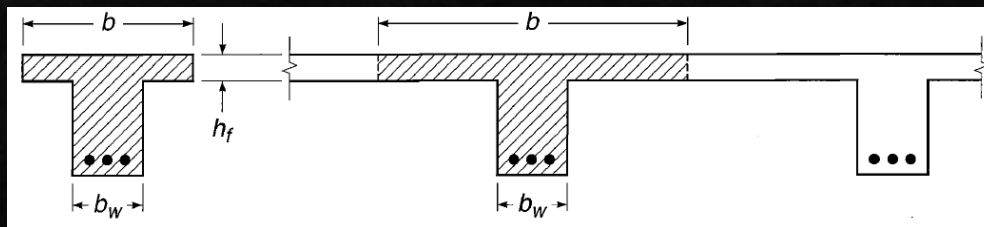
Flange location	Effective overhanging flange width, beyond face of web	
Each side of web	Least of:	$8h$
		$s_w/2$
		$l_n/8$
One side of web	Least of:	$6h$
		$s_w/2$
		$l_n/12$





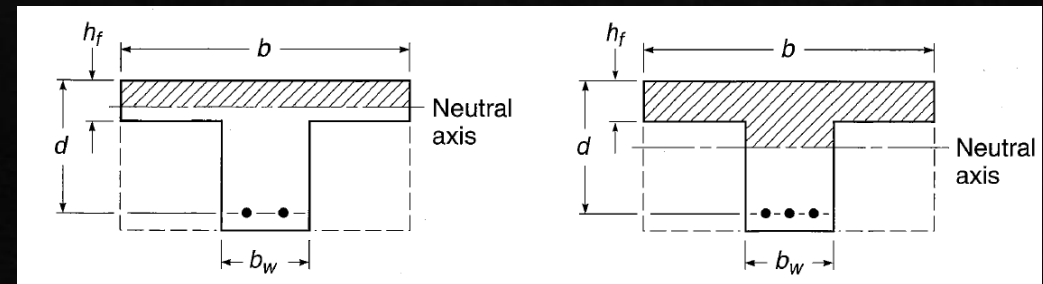
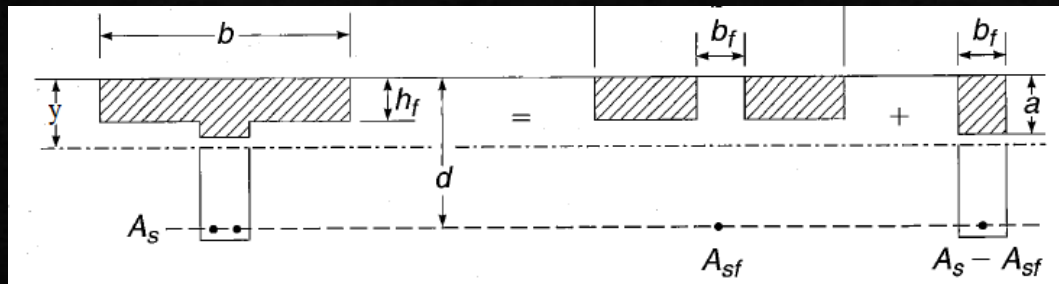
# What are T-section beams

- ◇ In some cases, engineers choose a T-shaped cross-section to increase the available compression area in the beam.
- ◇ The ACI code requires :
  - ◇ Flange thickness  $\geq 0.5b_w$
  - ◇ Effective flange width  $\leq 4b_w$

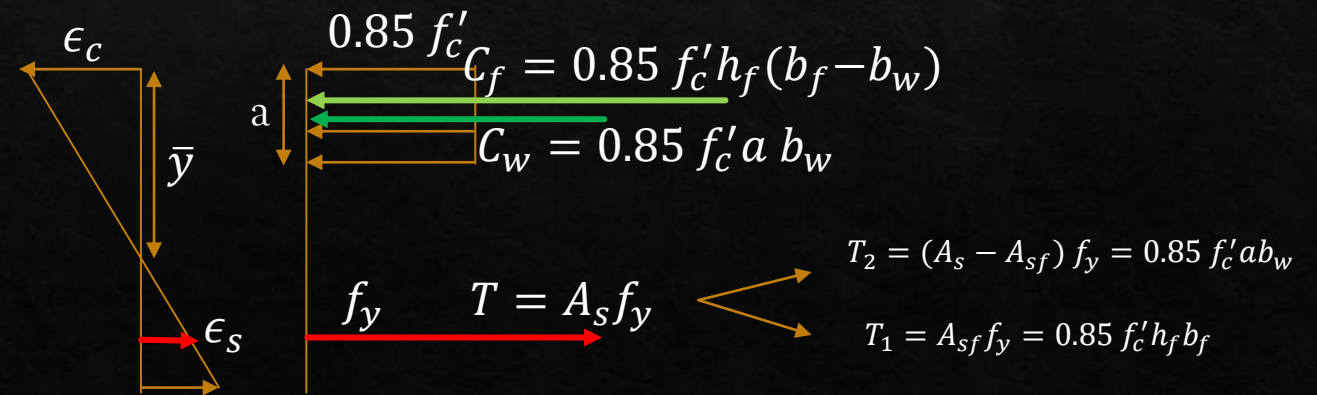
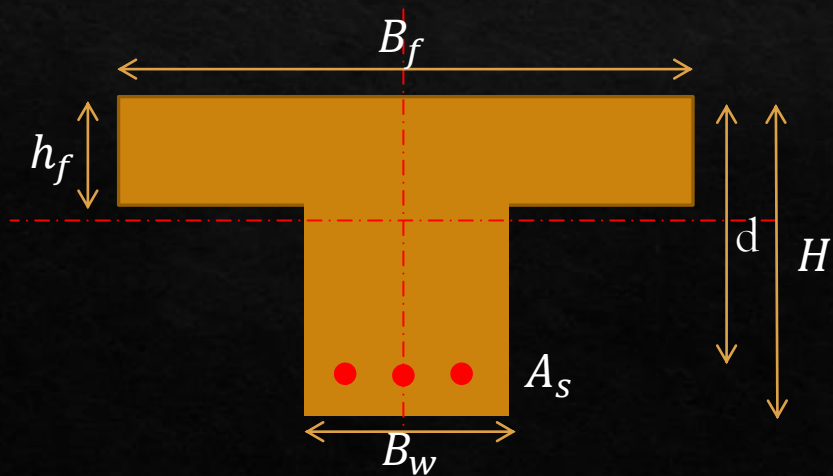
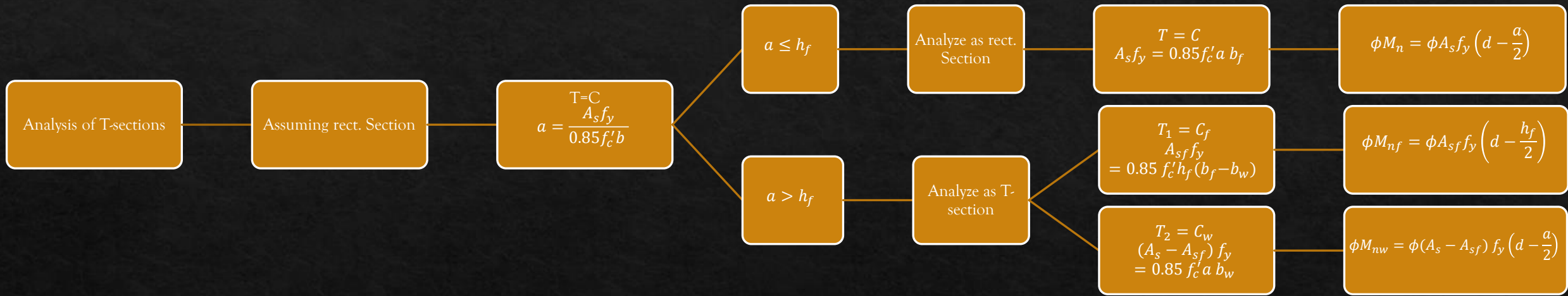


# Analysis of T-sections

- ◇ The N.A. of the beam may lie either in the FLANGE or in the WEB.
- ◇ This depends on the section geometry, material properties, and the amount of tensile steel.
- ◇ If  $N.A. \leq h_f$ : the beam can be analyzed as a rectangular section with width  $B_f$  and depth  $H$ .
  - ◇ WHY?
- ◇ If  $N.A. \geq h_f$ : the compression area is divided into two parts
  - ◇ The first part is the flange over-hang from each side which is coupled with part of the tension steel ( $A_{sf}$ )
  - ◇ The second Part is the portion of the Web in compression which is coupled with the rest of the tension steel ( $A_s - A_{sf}$ )
- ◇ **What is the Direction of the moment?? (+ or -)**



# Analysis of T-sections





# Analysis of T-sections

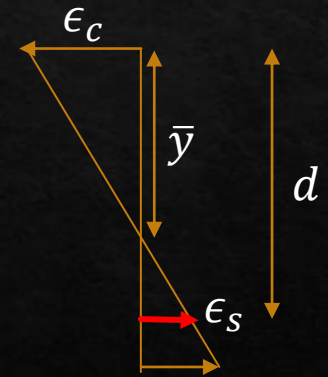
## ◆ Tension Reinforcement limits

- ◆ Minimum reinforcement remains the same ( $\rho_w > \rho_{min}$ )
- ◆ Maximum reinforcement allowed by ACI code still maintains a tension strain in steel  $\epsilon_t \geq 0.004$ 
  - ◆ We can calculate and compare the strain in the tension steel with the limit from the strain distribution

$$\epsilon_s = \epsilon_u \frac{d - \bar{y}}{\bar{y}} \geq 0.004$$

- ◆ Or we can use this formula (derived from strain distribution and section equilibrium)

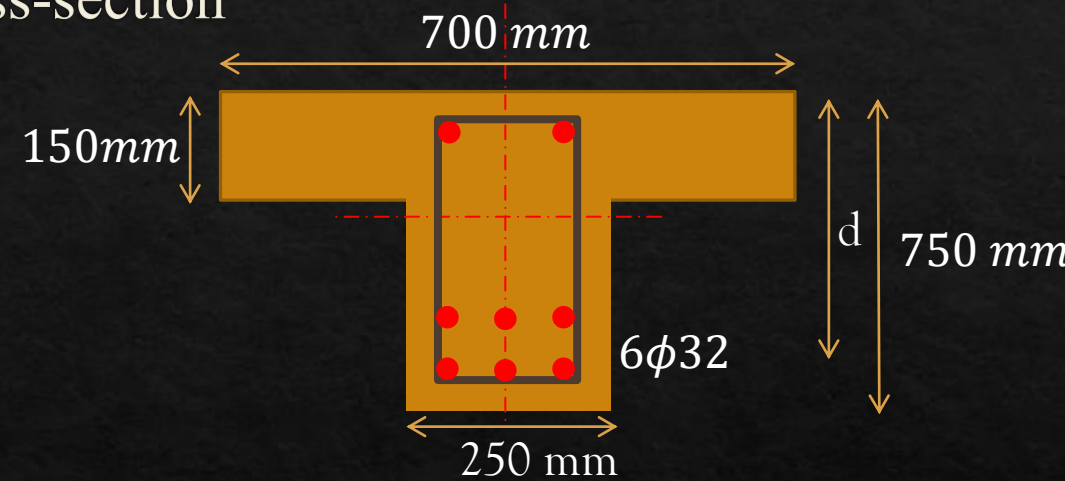
$$\bar{\rho}_{0.004} = \rho_{0.004} + \rho_f$$



# Analysis of T-sections

Example: Calculate the Moment capacity of the given cross-section

$$f_y = 420 \text{ MPa} \dots \dots f'_c = 21 \text{ MPa}$$





# Analysis of T-sections

## Example: Design

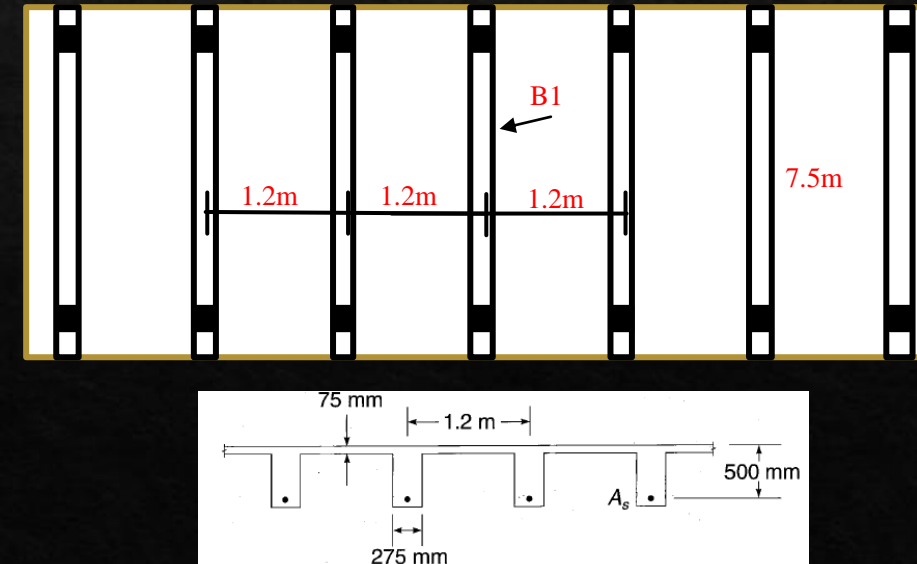
The floor system shown, consists of a 75mm concrete slab supported by continuous beams with 7.5 m span, and 1.2m center to center spacing. The Web dimensions were determined using the negative moment. Design the interior beam B1 indicated below knowing that the ultimate positive moment ( $M_u = 750 \text{ kN.m}$ )

$$f_y = 420 \text{ MPa} \dots \dots f'_c = 21 \text{ MPa}$$

$$b_e = \min \left\{ \begin{array}{l} 2(8h) + b_w = 1475 \text{ mm} \\ 2 \left( \frac{s_w - b_w}{2} \right) + b_w = 1200 \text{ mm} \leftarrow \\ 2 \left( \frac{l_n}{8} \right) + b_w = 2150 \text{ mm} \end{array} \right.$$

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# Arbitrary cross-sections

